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MULTIMEDIA UNIVERSITY

SUPPLEMENTARY EXAMINATION

TRIMESTER 1, 2015/2016

EMT2036 – ENGINEERING MATHEMATICS III
(All Sections / All Groups)

17 NOV 2015
9.00 AM – 11.00 AM
(2 HOURS)

GENERAL INSTRUCTIONS:

1. This exam paper consists of **3 pages** with **4 questions only**.
 2. Each question is worth **25 marks**. Attempt **ALL** questions.
 3. The required statistical distribution tables are provided in the appendix.
 4. Write all your answers in the answer booklet provided. **Show all relevant steps** to obtain maximum marks.
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Question 1

- (a) Solve the following set of equations using the Gauss-Jordan Elimination method:

$$2x + 2y + 4z = 18$$

$$x + 3y + 2z = 13$$

$$3x + y + 3z = 14.$$

[13 marks]

- (b) The eigenvalues of matrix $A = \begin{pmatrix} 1 & 2 \\ 3 & 2 \end{pmatrix}$ are -1 and 4 and the corresponding eigenvectors are $\begin{pmatrix} -1 \\ 1 \end{pmatrix}$ and $\begin{pmatrix} 2 \\ 3 \end{pmatrix}$. Find the general solution of the system

$$x_1' = x_1 + 2x_2$$

$$x_2' = 3x_1 + 2x_2$$

by using the given eigenvalues and eigenvectors of the coefficient matrix. Then find a solution satisfying the boundary conditions $x_1(0) = 0$ and $x_2(0) = 4$.

[12 marks]

Question 2

- (a) Find the volume of the solid bounded by the surfaces $x + y + z = 4$, $x = 0$, $y = 0$ and $z = 0$.

[15 marks]

- (b) Use the Divergence Theorem to find the outward flux of the vector field $\mathbf{F}(x, y, z) = x\mathbf{i} + y\mathbf{j} + z\mathbf{k}$ across the surface of the solid enclosed by the paraboloid $z = 1 - x^2 - y^2$ and the xy -plane.

[10 marks]

Continued...

Question 3

- (a) Evaluate $\int_C (x^2 + y^2)dx - xdy$ where C is the arc of a unit circle traversed counterclockwise from $(1,0)$ to $(0,1)$.

[5 marks]

- (b) Use Green's Theorem to compute $\oint_C x^2ydx + (y + xy^2)dy$ where C is the boundary of the region enclosed by $y = x^2$ and $x = y^2$.

[7 marks]

- (c) By applying Stokes' Theorem, evaluate $\oint_C \mathbf{F} \cdot d\mathbf{r}$ where $\mathbf{F} = (x - y)\mathbf{i} + (y - z)\mathbf{j} + (z - x)\mathbf{k}$ and C is the boundary of the plane $x + y + z = 1$ in the first octant with positive orientation.

[13 marks]

Question 4

- (a) An ice cream seller claims that the four flavours that he sells, which are chocolate, vanilla, strawberry and mint, are equally popular. From 200 observations of flavours selected by customers, the observed frequencies are 60 for chocolate, 46 for vanilla, 43 for strawberry and 51 for mint.

- (i) Test at a 0.05 level of significance whether the claim is true.

[10 marks]

- (ii) Find the 95% confidence interval for the proportion of customers selecting chocolate flavour.

[7 marks]

- (b) A service centre claims that the average waiting time at the centre is less than 30 minutes. To test the hypothesis that $\mu = 30$ minutes against the alternative that $\mu < 30$ minutes, a random sample of 60 samples are observed. The standard deviation is 16 minutes. The critical region is defined to be $\bar{x} < 29$.

- (i) Find the probability of committing a type I error.

[4 marks]

- (ii) Find the probability of committing a type II error for the alternative $\mu = 28.5$ minutes.

[4 marks]

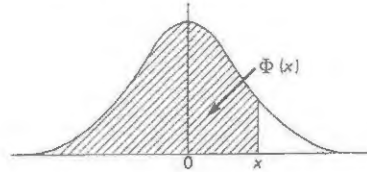
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Appendix

TABLE 4. THE NORMAL DISTRIBUTION FUNCTION

The function tabulated is $\Phi(x) = \frac{1}{\sqrt{2\pi}} \int_{-\infty}^x e^{-t^2/2} dt$. $\Phi(x)$ is

the probability that a random variable, normally distributed with zero mean and unit variance, will be less than or equal to x . When $x < 0$ use $\Phi(x) = 1 - \Phi(-x)$, as the normal distribution with zero mean and unit variance is symmetric about zero.



x	$\Phi(x)$	x	$\Phi(x)$	x	$\Phi(x)$	x	$\Phi(x)$	x	$\Phi(x)$	x	$\Phi(x)$
0.00	0.5000	0.40	0.6554	0.80	0.7881	1.20	0.8849	1.60	0.9452	2.00	0.97725
0.01	5040	0.41	6591	0.81	7910	1.21	8869	1.61	9463	2.01	97778
0.02	5080	0.42	6628	0.82	7939	1.22	8888	1.62	9474	2.02	97831
0.03	5120	0.43	6664	0.83	7967	1.23	8907	1.63	9484	2.03	97882
0.04	5160	0.44	6700	0.84	7995	1.24	8925	1.64	9495	2.04	97932
0.05	5199	0.45	6736	0.85	8023	1.25	8944	1.65	9505	2.05	97982
0.06	5239	0.46	6772	0.86	8051	1.26	8962	1.66	9515	2.06	98030
0.07	5279	0.47	6808	0.87	8078	1.27	8980	1.67	9525	2.07	98077
0.08	5319	0.48	6844	0.88	8106	1.28	8997	1.68	9535	2.08	98124
0.09	5359	0.49	6879	0.89	8133	1.29	9015	1.69	9545	2.09	98169
0.10	5398	0.50	6915	0.90	8159	1.30	9032	1.70	9554	2.10	98214
0.11	5438	0.51	6950	0.91	8186	1.31	9049	1.71	9564	2.11	98257
0.12	5478	0.52	6985	0.92	8212	1.32	9066	1.72	9573	2.12	98300
0.13	5517	0.53	7019	0.93	8238	1.33	9082	1.73	9582	2.13	98341
0.14	5557	0.54	7054	0.94	8264	1.34	9099	1.74	9591	2.14	98382
0.15	5596	0.55	7088	0.95	8289	1.35	9115	1.75	9599	2.15	98422
0.16	5636	0.56	7123	0.96	8315	1.36	9131	1.76	9608	2.16	98461
0.17	5675	0.57	7157	0.97	8340	1.37	9147	1.77	9616	2.17	98500
0.18	5714	0.58	7190	0.98	8365	1.38	9162	1.78	9625	2.18	98537
0.19	5753	0.59	7224	0.99	8389	1.39	9177	1.79	9633	2.19	98574
0.20	5793	0.60	7257	1.00	8413	1.40	9192	1.80	9641	2.20	98610
0.21	5832	0.61	7291	0.01	8438	1.41	9207	1.81	9649	2.21	98645
0.22	5871	0.62	7324	0.02	8461	1.42	9222	1.82	9656	2.22	98679
0.23	5910	0.63	7357	0.03	8485	1.43	9236	1.83	9664	2.23	98713
0.24	5948	0.64	7389	0.04	8508	1.44	9251	1.84	9671	2.24	98745
0.25	5987	0.65	7422	1.05	8531	1.45	9265	1.85	9678	2.25	98778
0.26	6026	0.66	7454	0.06	8554	1.46	9279	1.86	9686	2.26	98809
0.27	6064	0.67	7486	0.07	8577	1.47	9292	1.87	9693	2.27	98840
0.28	6103	0.68	7517	0.08	8599	1.48	9306	1.88	9699	2.28	98870
0.29	6141	0.69	7549	0.09	8621	1.49	9319	1.89	9706	2.29	98899
0.30	6179	0.70	7580	1.10	8643	1.50	9332	1.90	9713	2.30	98928
0.31	6217	0.71	7611	0.11	8665	1.51	9345	1.91	9719	2.31	98956
0.32	6255	0.72	7642	0.12	8686	1.52	9357	1.92	9726	2.32	98983
0.33	6293	0.73	7673	0.13	8708	1.53	9370	1.93	9732	2.33	99010
0.34	6331	0.74	7704	0.14	8729	1.54	9382	1.94	9738	2.34	99036
0.35	6368	0.75	7734	1.15	8749	1.55	9394	1.95	9744	2.35	99061
0.36	6406	0.76	7764	0.16	8770	1.56	9406	1.96	9750	2.36	99086
0.37	6443	0.77	7794	0.17	8790	1.57	9418	1.97	9756	2.37	99111
0.38	6480	0.78	7823	0.18	8810	1.58	9429	1.98	9761	2.38	99134
0.39	6517	0.79	7852	0.19	8830	1.59	9441	1.99	9767	2.39	99158
0.40	6554	0.80	7881	1.20	8849	1.60	9452	2.00	9772	2.40	99180

x	$\Phi(x)$	x	$\Phi(x)$	x	$\Phi(x)$	x	$\Phi(x)$	x	$\Phi(x)$	x	$\Phi(x)$
2.40	0.99180	2.55	0.99461	2.70	0.99653	2.85	0.99781	3.00	0.99865	3.15	0.99918
41	.99202	56	.99477	71	.99664	86	.99788	01	.99869	16	.99921
42	.99224	57	.99492	72	.99674	87	.99795	02	.99874	17	.99924
43	.99245	58	.99506	73	.99683	88	.99801	03	.99878	18	.99926
44	.99266	59	.99520	74	.99693	89	.99807	04	.99882	19	.99929
2.45	0.99286	2.60	0.99534	2.75	0.99702	2.90	0.99813	3.05	0.99886	3.20	0.99931
46	.99305	61	.99547	76	.99711	91	.99819	06	.99889	21	.99934
47	.99324	62	.99560	77	.99720	92	.99825	07	.99893	22	.99936
48	.99343	63	.99573	78	.99728	93	.99831	08	.99896	23	.99938
49	.99361	64	.99585	79	.99736	94	.99836	09	.99900	24	.99940
2.50	0.99379	2.65	0.99598	2.80	0.99744	2.95	0.99841	3.10	0.99903	3.25	0.99942
51	.99396	66	.99609	81	.99752	96	.99846	11	.99906	26	.99944
52	.99413	67	.99621	82	.99760	97	.99851	12	.99910	27	.99946
53	.99430	68	.99632	83	.99767	98	.99856	13	.99913	28	.99948
54	.99446	69	.99643	84	.99774	99	.99861	14	.99916	29	.99950
2.55	0.99461	2.70	0.99653	2.85	0.99781	3.00	0.99865	3.15	0.99918	3.30	0.99952

The critical table below gives on the left the range of values of x for which $\Phi(x)$ takes the value on the right, correct to the last figure given; in critical cases, take the upper of the two values of $\Phi(x)$ indicated.

3.075	0.9990	3.263	0.9994	3.731	0.99990	3.916	0.99995
3.105	0.9991	3.320	0.9995	3.759	0.99991	3.976	0.99996
3.138	0.9992	3.389	0.9996	3.791	0.99992	4.055	0.99997
3.174	0.9993	3.480	0.9997	3.826	0.99993	4.173	0.99998
3.215	0.9994	3.615	0.9998	3.867	0.99994	4.417	0.99999
					0.99995		1.00000

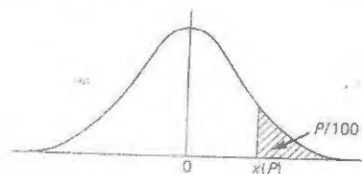
When $x > 3.3$ the formula $1 - \Phi(x) \doteq \frac{e^{-x^2}}{x\sqrt{2\pi}} \left[1 - \frac{1}{x^2} + \frac{3}{x^4} - \frac{15}{x^6} + \frac{105}{x^8} \right]$ is very accurate, with relative error less than $945/x^{10}$.

TABLE 5. PERCENTAGE POINTS OF THE NORMAL DISTRIBUTION

This table gives percentage points $x(P)$ defined by the equation

$$\frac{P}{100} = \frac{1}{\sqrt{2\pi}} \int_{x(P)}^{\infty} e^{-t^2/2} dt.$$

If X is a variable, normally distributed with zero mean and unit variance, $P/100$ is the probability that $X \geq x(P)$. The lower P per cent points are given by symmetry as $-x(P)$, and the probability that $|X| \geq x(P)$ is $2P/100$.



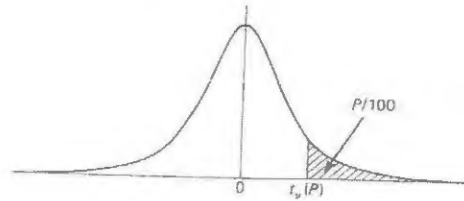
P	$x(P)$	P	$x(P)$	P	$x(P)$	P	$x(P)$	P	$x(P)$	P	$x(P)$
50	0.0000	5.0	1.6449	3.0	1.8808	2.0	2.0537	1.0	2.3263	0.10	3.0902
45	0.1257	4.8	1.6646	2.9	1.8957	1.9	2.0749	0.9	2.3656	0.09	3.1214
40	0.2533	4.6	1.6849	2.8	1.9110	1.8	2.0969	0.8	2.4089	0.08	3.1559
35	0.3853	4.4	1.7060	2.7	1.9268	1.7	2.1201	0.7	2.4573	0.07	3.1947
30	0.5244	4.2	1.7279	2.6	1.9431	1.6	2.1444	0.6	2.5121	0.06	3.2389
25	0.6745	4.0	1.7507	2.5	1.9600	1.5	2.1701	0.5	2.5758	0.05	3.2905
20	0.8416	3.8	1.7744	2.4	1.9774	1.4	2.1973	0.4	2.6521	0.04	3.7190
15	1.0364	3.6	1.7991	2.3	1.9954	1.3	2.2262	0.3	2.7478	0.005	3.8906
10	1.2816	3.4	1.8250	2.2	2.0141	1.2	2.2571	0.2	2.8782	0.001	4.2649
5	1.6449	3.2	1.8522	2.1	2.0335	1.1	2.2904	0.1	3.0902	0.0005	4.4172

TABLE 10. PERCENTAGE POINTS OF THE *t*-DISTRIBUTION

This table gives percentage points $t_p(P)$ defined by the equation

$$\frac{P}{100} = \frac{1}{\sqrt{\pi}} \frac{\Gamma(\frac{1}{2}\nu + \frac{1}{2})}{\Gamma(\frac{1}{2}\nu)} \int_{t_p(P)}^{\infty} \frac{dt}{(1+t^2/\nu)^{\frac{1}{2}(\nu+1)}}$$

Let X_1 and X_2 be independent random variables having a normal distribution with zero mean and unit variance and a χ^2 -distribution with ν degrees of freedom respectively; then $t = X_1/\sqrt{X_2/\nu}$ has Student's *t*-distribution with ν degrees of freedom, and the probability that $t \geq t_p(P)$ is $P/100$. The lower percentage points are given by symmetry as $-t_p(P)$, and the probability that $|t| \geq t_p(P)$ is $2P/100$.



The limiting distribution of *t* as ν tends to infinity is the normal distribution with zero mean and unit variance. When ν is large interpolation in ν should be harmonic.

P	40	30	25	20	15	10	5	2.5	1	0.5	0.1	0.05
$\nu = 1$	0.3249	0.7265	1.0000	1.3764	1.963	3.078	6.314	12.71	31.82	63.66	318.3	636.6
2	0.2887	0.6172	0.8165	1.0607	1.386	1.886	2.920	4.303	6.965	9.925	22.33	31.60
3	0.2767	0.5844	0.7649	0.9785	1.250	1.638	2.353	3.182	4.541	5.841	10.21	12.92
4	0.2707	0.5686	0.7407	0.9410	1.190	1.533	2.132	2.776	3.747	4.604	7.173	8.610
5	0.2672	0.5594	0.7267	0.9195	1.156	1.476	2.015	2.571	3.365	4.032	5.893	6.869
6	0.2648	0.5534	0.7176	0.9057	1.134	1.440	1.943	2.447	3.143	3.707	5.208	5.959
7	0.2632	0.5491	0.7111	0.8960	1.119	1.415	1.895	2.365	2.998	3.499	4.785	5.408
8	0.2619	0.5459	0.7064	0.8889	1.108	1.397	1.860	2.306	2.896	3.355	4.501	5.041
9	0.2610	0.5435	0.7027	0.8834	1.100	1.383	1.833	2.262	2.821	3.250	4.297	4.781
10	0.2602	0.5415	0.6998	0.8791	1.093	1.372	1.812	2.228	2.764	3.169	4.144	4.587
11	0.2596	0.5399	0.6974	0.8753	1.088	1.363	1.796	2.201	2.718	3.106	4.025	4.437
12	0.2590	0.5386	0.6955	0.8726	1.083	1.356	1.782	2.179	2.681	3.055	3.930	4.318
13	0.2586	0.5375	0.6938	0.8702	1.079	1.350	1.771	2.160	2.650	3.012	3.852	4.221
14	0.2582	0.5366	0.6924	0.8681	1.076	1.345	1.761	2.145	2.624	2.977	3.787	4.140
15	0.2579	0.5357	0.6912	0.8662	1.074	1.341	1.753	2.131	2.602	2.947	3.733	4.073
16	0.2576	0.5350	0.6901	0.8647	1.071	1.337	1.746	2.120	2.583	2.921	3.686	4.015
17	0.2573	0.5344	0.6892	0.8633	1.069	1.333	1.740	2.110	2.567	2.898	3.646	3.965
18	0.2571	0.5338	0.6884	0.8620	1.067	1.330	1.734	2.101	2.552	2.878	3.610	3.922
19	0.2569	0.5333	0.6876	0.8610	1.066	1.328	1.729	2.093	2.539	2.861	3.579	3.883
20	0.2567	0.5329	0.6870	0.8600	1.064	1.325	1.725	2.086	2.528	2.845	3.552	3.850
21	0.2566	0.5325	0.6864	0.8591	1.063	1.323	1.721	2.080	2.518	2.831	3.527	3.819
22	0.2564	0.5321	0.6858	0.8583	1.061	1.321	1.717	2.074	2.508	2.819	3.505	3.792
23	0.2563	0.5317	0.6853	0.8575	1.060	1.319	1.714	2.069	2.500	2.807	3.485	3.768
24	0.2562	0.5314	0.6848	0.8569	1.059	1.318	1.711	2.064	2.492	2.797	3.467	3.745
25	0.2561	0.5312	0.6844	0.8562	1.058	1.316	1.708	2.060	2.485	2.787	3.450	3.725
26	0.2560	0.5309	0.6840	0.8557	1.058	1.315	1.706	2.056	2.479	2.779	3.435	3.707
27	0.2559	0.5306	0.6837	0.8551	1.057	1.314	1.703	2.052	2.473	2.771	3.421	3.690
28	0.2558	0.5304	0.6834	0.8546	1.056	1.313	1.701	2.048	2.467	2.763	3.408	3.674
29	0.2557	0.5302	0.6830	0.8542	1.055	1.311	1.699	2.045	2.462	2.756	3.396	3.659
30	0.2556	0.5300	0.6828	0.8538	1.055	1.310	1.697	2.042	2.457	2.750	3.385	3.646
32	0.2555	0.5297	0.6822	0.8530	1.054	1.309	1.694	2.037	2.449	2.738	3.365	3.622
34	0.2553	0.5294	0.6818	0.8523	1.052	1.307	1.691	2.032	2.441	2.728	3.348	3.601
36	0.2552	0.5291	0.6814	0.8517	1.052	1.306	1.688	2.028	2.434	2.719	3.333	3.582
38	0.2551	0.5288	0.6810	0.8512	1.051	1.304	1.686	2.024	2.429	2.712	3.319	3.566
40	0.2550	0.5286	0.6807	0.8507	1.050	1.303	1.684	2.021	2.423	2.704	3.307	3.551
50	0.2547	0.5278	0.6794	0.8489	1.047	1.299	1.676	2.009	2.403	2.678	3.261	3.496
60	0.2545	0.5272	0.6786	0.8477	1.045	1.296	1.671	2.000	2.390	2.660	3.232	3.460
120	0.2539	0.5258	0.6765	0.8446	1.041	1.289	1.658	1.980	2.358	2.617	3.160	3.373
∞	0.2533	0.5244	0.6745	0.8416	1.036	1.282	1.645	1.960	2.326	2.576	3.090	3.291

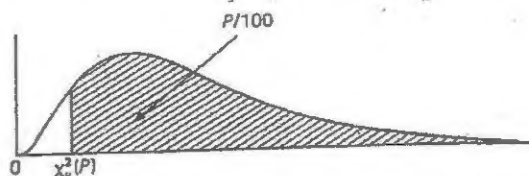
TABLE 8. PERCENTAGE POINTS OF THE χ^2 -DISTRIBUTION

This table gives percentage points $\chi^2_\nu(P)$ defined by the equation

$$\frac{P}{100} = \frac{1}{2^{\nu/2} \Gamma(\frac{\nu}{2})} \int_{\chi^2_\nu(P)}^{\infty} x^{\nu/2-1} e^{-x/2} dx.$$

If X is a variable distributed as χ^2 with ν degrees of freedom, $P/100$ is the probability that $X \geq \chi^2_\nu(P)$.

For $\nu > 100$, $\sqrt{2X}$ is approximately normally distributed with mean $\sqrt{2\nu} - 1$ and unit variance.



(The above shape applies for $\nu \geq 3$ only. When $\nu < 3$ the mode is at the origin.)

P	99.95	99.9	99.5	99	97.5	95	90	80	70	60
$\nu = 1$	0.003927	0.001571	0.003927	0.001571	0.009821	0.003932	0.01579	0.06418	0.1485	0.2750
2	0.001000	0.002001	0.01003	0.02010	0.05064	0.1026	0.2107	0.4463	0.7133	1.022
3	0.01528	0.02430	0.07172	0.1148	0.2158	0.3528	0.5844	1.005	1.424	1.869
4	0.06392	0.09080	0.2070	0.2971	0.4844	0.7107	1.064	1.649	2.195	2.753
5	0.1581	0.2102	0.4117	0.5543	0.8312	1.145	1.610	2.343	3.000	3.655
6	0.2994	0.3811	0.6757	0.8721	1.237	1.635	2.204	3.070	3.828	4.570
7	0.4849	0.5985	0.9893	1.239	1.690	2.167	2.833	3.822	4.671	5.493
8	0.7104	0.8571	1.344	1.646	2.180	2.733	3.490	4.594	5.527	6.423
9	0.9717	1.152	1.735	2.088	2.700	3.325	4.168	5.380	6.393	7.357
10	1.265	1.479	2.156	2.558	3.247	3.940	4.865	6.179	7.267	8.295
11	1.587	1.834	2.603	3.053	3.816	4.575	5.578	6.989	8.148	9.237
12	1.934	2.214	3.074	3.571	4.404	5.226	6.304	7.807	9.034	10.18
13	2.305	2.617	3.565	4.107	5.009	5.892	7.042	8.634	9.926	11.13
14	2.697	3.041	4.075	4.660	5.629	6.571	7.790	9.467	10.82	12.08
15	3.108	3.483	4.601	5.229	6.262	7.261	8.547	10.31	11.72	13.03
16	3.536	3.942	5.142	5.812	6.908	7.962	9.312	11.15	12.62	13.98
17	3.980	4.416	5.697	6.408	7.564	8.672	10.09	12.00	13.53	14.94
18	4.439	4.905	6.265	7.015	8.231	9.390	10.86	12.86	14.44	15.89
19	4.912	5.407	6.844	7.633	8.907	10.12	11.65	13.72	15.35	16.85
20	5.398	5.921	7.434	8.260	9.591	10.85	12.44	14.58	16.27	17.81
21	5.896	6.447	8.034	8.897	10.28	11.59	13.24	15.44	17.18	18.77
22	6.404	6.983	8.643	9.542	10.98	12.34	14.04	16.31	18.10	19.73
23	6.924	7.529	9.260	10.20	11.69	13.09	14.85	17.19	19.02	20.69
24	7.453	8.085	9.886	10.86	12.40	13.85	15.66	18.06	19.94	21.65
25	7.991	8.649	10.52	11.52	13.12	14.61	16.47	18.94	20.87	22.62
26	8.538	9.222	11.16	12.20	13.84	15.38	17.29	19.82	21.79	23.58
27	9.093	9.803	11.81	12.88	14.57	16.15	18.11	20.70	22.72	24.54
28	9.656	10.39	12.46	13.56	15.31	16.93	18.94	21.59	23.65	25.51
29	10.23	10.99	13.12	14.26	16.05	17.71	19.77	22.48	24.58	26.48
30	10.80	11.59	13.79	14.95	16.79	18.49	20.60	23.36	25.51	27.44
32	11.98	12.81	15.13	16.36	18.29	20.07	22.27	25.15	27.37	29.38
34	13.18	14.06	16.50	17.79	19.81	21.66	23.95	26.94	29.24	31.31
36	14.40	15.32	17.89	19.23	21.34	23.27	25.64	28.73	31.12	33.25
38	15.64	16.61	19.29	20.69	22.88	24.88	27.34	30.54	32.99	35.19
40	16.91	17.92	20.71	22.16	24.43	26.51	29.05	32.34	34.87	37.13
50	23.46	24.67	27.99	29.71	32.36	34.76	37.69	41.45	44.31	46.86
60	30.34	31.74	35.53	37.48	40.48	43.19	46.46	50.64	53.81	56.62
70	37.47	39.04	43.28	45.44	48.76	51.74	55.33	59.90	63.35	66.40
80	44.79	46.52	51.17	53.54	57.15	60.39	64.28	69.21	72.92	76.19
90	52.28	54.16	59.20	61.75	65.65	69.13	73.29	78.56	82.51	85.99
100	59.90	61.92	67.33	70.06	74.22	77.93	82.36	87.95	92.13	95.81

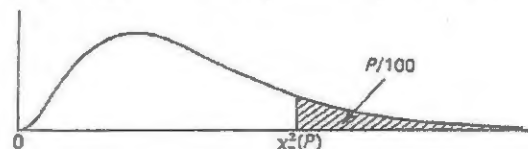
TABLE 8. PERCENTAGE POINTS OF THE χ^2 -DISTRIBUTION

This table gives percentage points $\chi^2(P)$ defined by the equation

$$\frac{P}{100} = \frac{1}{2^{v/2} \Gamma(\frac{v}{2})} \int_{\chi^2(P)}^{\infty} x^{v/2-1} e^{-x/2} dx.$$

If X is a variable distributed as χ^2 with ν degrees of freedom, $P/100$ is the probability that $X \geq \chi^2(P)$.

For $\nu > 100$, $\sqrt{2}X$ is approximately normally distributed with mean $\sqrt{2\nu} - 1$ and unit variance.



(The above shape applies for $\nu \geq 3$ only. When $\nu < 3$ the mode is at the origin.)

P	50	40	30	20	10	5	2.5	1	0.5	0.1	0.05
$\nu = 1$	0.4549	0.7083	1.074	1.642	2.706	3.841	5.024	6.635	7.879	10.83	12.12
2	1.386	1.833	2.408	3.219	4.605	5.991	7.378	9.210	10.60	13.82	15.20
3	2.366	2.946	3.665	4.642	6.251	7.815	9.348	11.34	12.84	16.27	17.73
4	3.357	4.045	4.878	5.989	7.779	9.488	11.14	13.28	14.86	18.47	20.00
5	4.351	5.132	6.064	7.289	9.236	11.07	12.83	15.09	16.75	20.52	22.11
6	5.348	6.211	7.231	8.558	10.64	12.59	14.45	16.81	18.55	22.46	24.10
7	6.346	7.283	8.383	9.803	12.02	14.07	16.01	18.48	20.28	24.32	26.02
8	7.344	8.351	9.524	11.03	13.36	15.51	17.53	20.09	21.95	26.12	27.87
9	8.343	9.414	10.66	12.24	14.68	16.92	19.02	21.67	23.59	27.88	29.67
10	9.342	10.47	11.78	13.44	15.99	18.31	20.48	23.21	25.19	29.59	31.42
11	10.34	11.53	12.90	14.63	17.28	19.68	21.92	24.72	26.76	31.26	33.14
12	11.34	12.58	14.01	15.81	18.55	21.03	23.34	26.22	28.30	32.91	34.82
13	12.34	13.64	15.12	16.98	19.81	22.36	24.74	27.69	29.82	34.53	36.48
14	13.34	14.69	16.22	18.15	21.06	23.68	26.12	29.14	31.32	36.12	38.11
15	14.34	15.73	17.32	19.31	22.31	25.00	27.49	30.58	32.80	37.70	39.72
16	15.34	16.78	18.42	20.47	23.54	26.30	28.85	32.00	34.27	39.25	41.31
17	16.34	17.82	19.51	21.61	24.77	27.59	30.19	33.41	35.72	40.79	42.88
18	17.34	18.87	20.60	22.76	25.99	28.87	31.53	34.81	37.16	42.31	44.43
19	18.34	19.91	21.69	23.90	27.20	30.14	32.85	36.19	38.58	43.82	45.97
20	19.34	20.95	22.77	25.04	28.41	31.41	34.17	37.57	40.00	45.31	47.50
21	20.34	21.99	23.86	26.17	29.62	32.67	35.48	38.93	41.40	46.80	49.01
22	21.34	23.03	24.94	27.30	30.81	33.92	36.78	40.29	42.80	48.27	50.51
23	22.34	24.07	26.02	28.43	32.01	35.17	38.08	41.64	44.18	49.73	52.00
24	23.34	25.11	27.10	29.55	33.20	36.42	39.36	42.98	45.56	51.18	53.48
25	24.34	26.14	28.17	30.68	34.38	37.65	40.65	44.31	46.93	52.62	54.95
26	25.34	27.18	29.25	31.79	35.56	38.89	41.92	45.64	48.29	54.05	56.41
27	26.34	28.21	30.32	32.91	36.74	40.11	43.19	46.96	49.64	55.48	57.86
28	27.34	29.25	31.39	34.03	37.92	41.34	44.46	48.28	50.99	56.89	59.30
29	28.34	30.28	32.46	35.14	39.09	42.56	45.72	49.59	52.34	58.30	60.73
30	29.34	31.32	33.53	36.25	40.26	43.77	46.98	50.89	53.67	59.70	62.16
32	31.34	33.38	35.66	38.47	42.58	46.19	49.48	53.49	56.33	62.49	65.00
34	33.34	35.44	37.80	40.68	44.90	48.60	51.97	56.06	58.96	65.25	67.80
36	35.34	37.50	39.92	42.88	47.21	51.00	54.44	58.62	61.58	67.99	70.59
38	37.34	39.56	42.05	45.08	49.51	53.38	56.90	61.16	64.18	70.70	73.35
40	39.34	41.62	44.16	47.27	51.81	55.76	59.34	63.69	66.77	73.40	76.09
50	49.33	51.89	54.72	58.16	63.17	67.50	71.42	76.15	79.49	86.66	89.56
60	59.33	62.13	65.23	68.97	74.40	79.08	83.30	88.38	91.95	99.61	102.7
70	69.33	72.36	75.69	79.71	85.53	90.53	95.02	100.4	104.2	112.3	115.6
80	79.33	82.57	86.12	90.41	96.58	101.9	106.6	112.3	116.3	124.8	128.3
90	89.33	92.76	96.52	101.1	107.6	113.1	118.1	124.1	128.3	137.2	140.8
100	99.33	102.9	106.9	111.7	118.5	124.3	129.6	135.8	140.2	149.4	153.2